

# **HOMs IN VELOCITY-OF-LIGHT SPOKE CAVITIES**

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and**

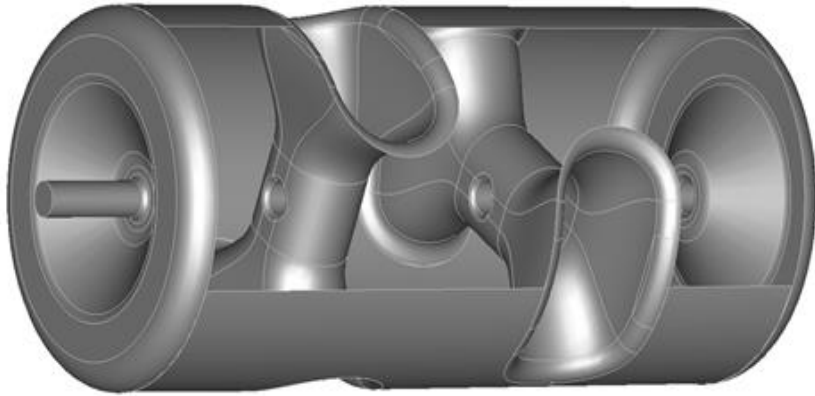
**Thomas Jefferson National Accelerator Facility**

# TOPICS COVERED TODAY...

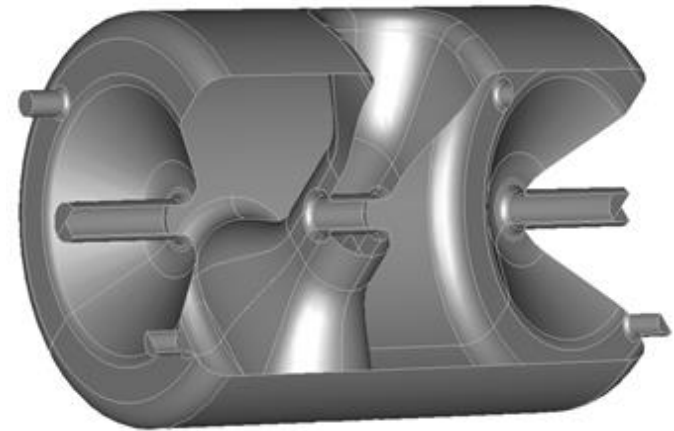
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- Introduction
- Mode Types
- $[R/Q]$ ,  $[R/Q]_T$  Calculations
- Velocity Dependence
- HOM Damping

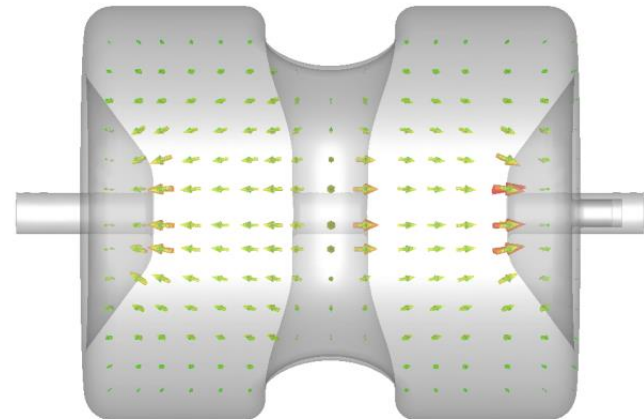
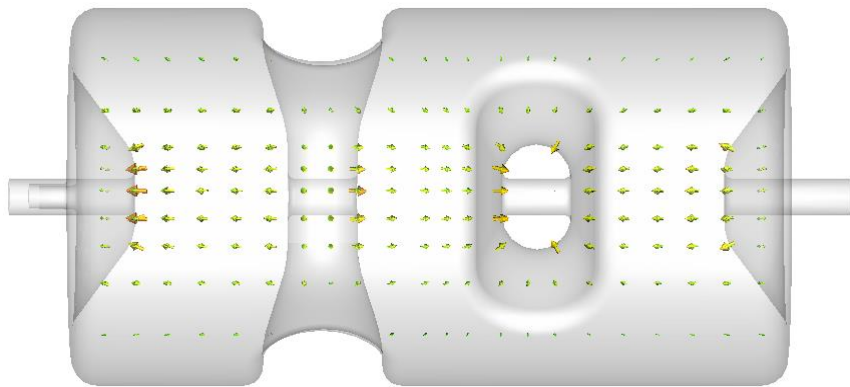
# HIGH-VELOCITY SPOKE CAVITIES



500 MHz,  $\beta_0 = 1$  double-spoke cavity



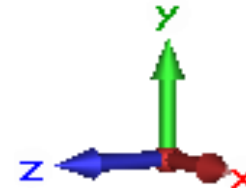
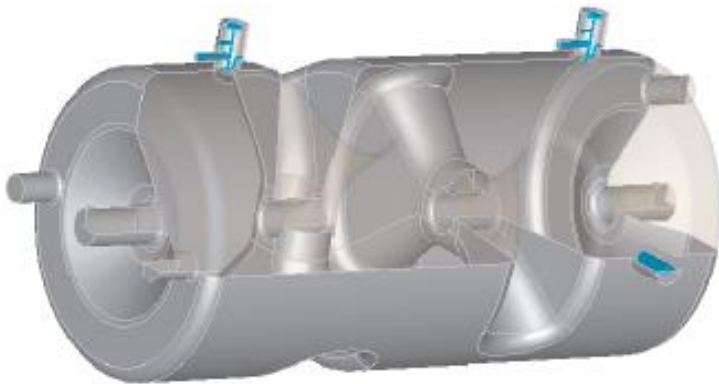
325 MHz,  $\beta_0 = 0.82$  single-spoke cavity



TEM-Class, Accelerating Cavities

# TERMINOLOGY

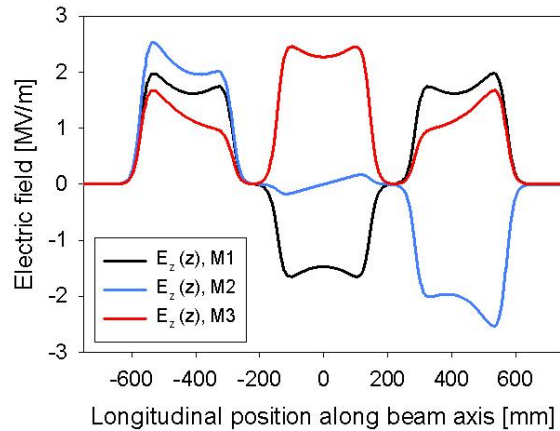
- The beam travels along the  $z$  axis. Transverse directions are  $x$  and  $y$ , which run parallel to the spoke(s).
- Accelerating modes are those where  $E_z(z)$ , along the beam axis, is greater than  $E_x(z)$  and  $E_y(z)$ .
- Deflecting modes are those where either  $E_x(z)$  or  $E_y(z)$  are greater than  $E_z(z)$ .
- $\phi$  is the phase between the particle and the rf fields. When considered in a calculation of  $[R/Q]$ ,  $[R/Q]_T$ , the value  $\phi$  of is that which maximizes the voltage.



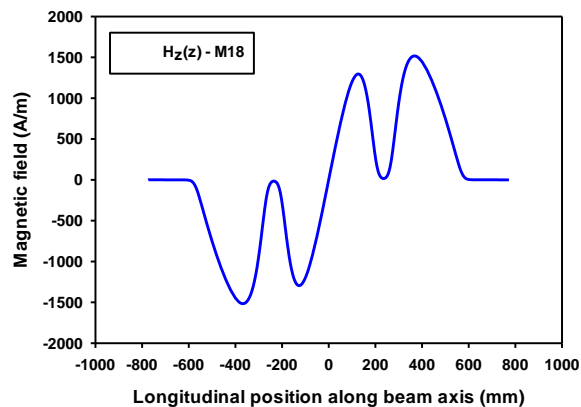
- 
- Introduction
  - **Mode Types**
  - $[R/Q]$ ,  $[R/Q]_T$  Calculations
  - Velocity Dependence
  - HOM Damping

# MODE TYPES (DOUBLE-SPOKE)

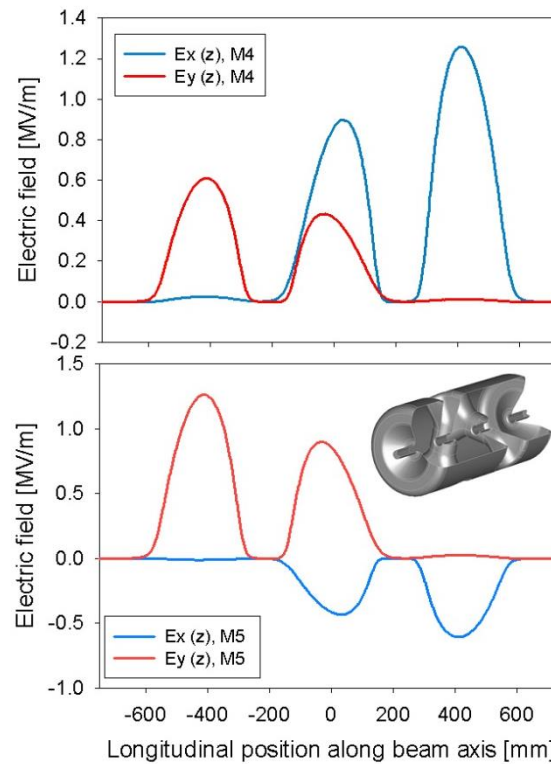
## Accelerating modes



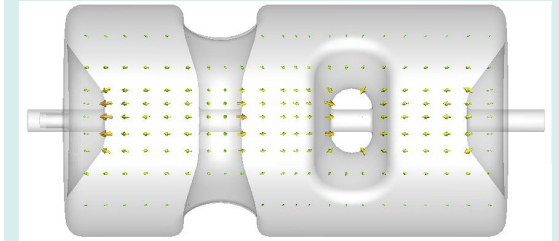
## TE-type modes



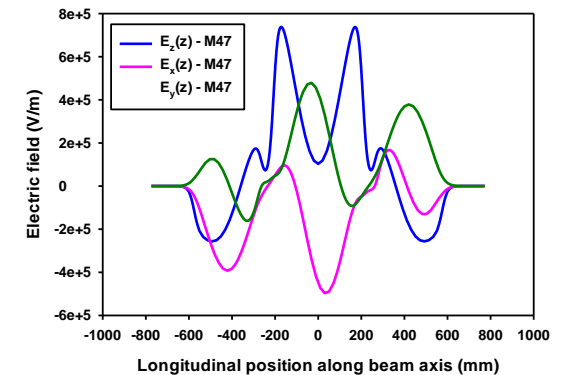
## Deflecting Modes (degenerate) modes



## Examples of modes for the 325 MHz cavity, $\beta_0 = 1$

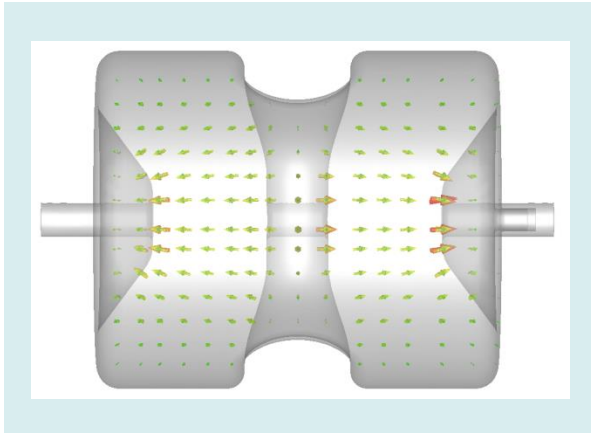
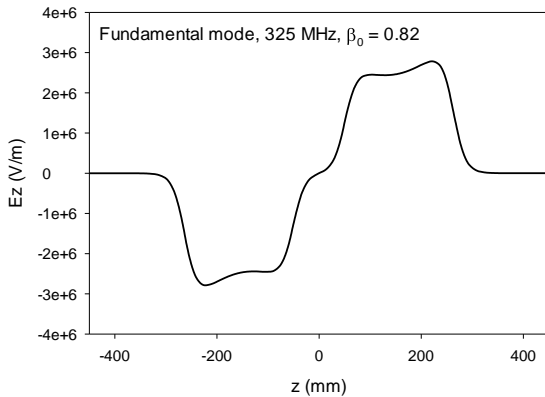


## Hybrid modes

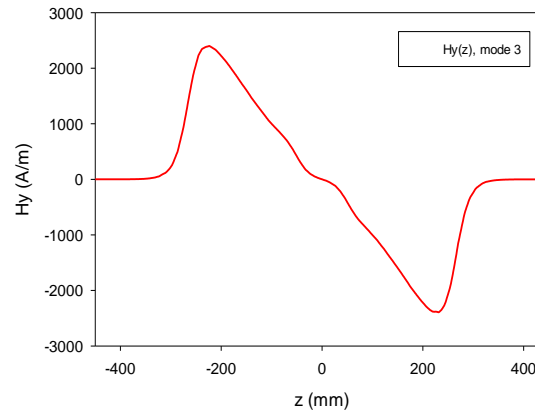
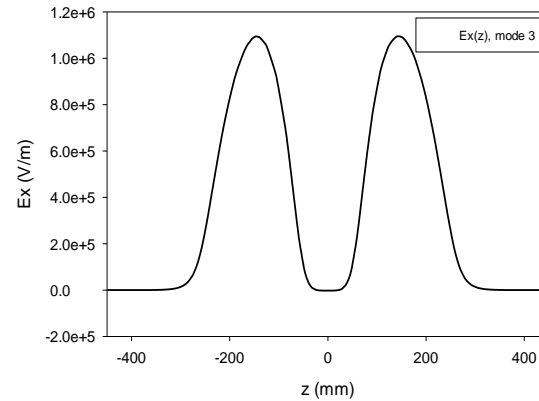


# MODE TYPES (SINGLE-SPOKE)

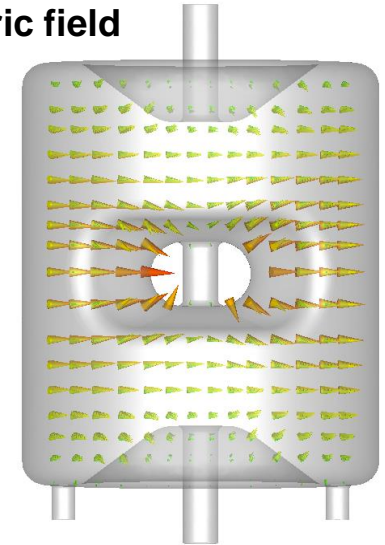
## Accelerating modes



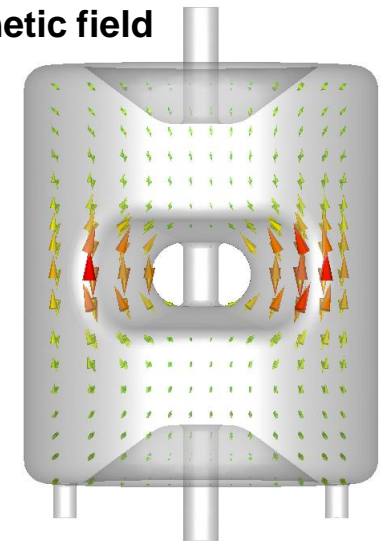
## Deflecting modes



## Electric field



## Magnetic field



- Introduction
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# CALCULATING [R/Q], [R/Q]<sub>T</sub>

## Accelerating Modes

$$\left(\frac{R}{Q}\right) = \frac{V_{acc}^2}{\omega_n U}$$

$$V_{acc} = \left| \int_{-\infty}^{\infty} E_z(z, r=0) \cos\left(\frac{\omega z}{\beta c} + \varphi\right) dz \right|$$

$$\left(\frac{R}{Q}\right) = \frac{\left| \int_{-\infty}^{\infty} E_z(z, r=0) \cos\left(\frac{\omega z}{\beta c} + \varphi\right) dz \right|^2}{\omega_n U} \Bigg|_{\max \varphi}$$

## Deflecting Modes

$$\left(\frac{R}{Q}\right)_{\perp} = \frac{\left| \int_{-\infty}^{+\infty} \left( \vec{E}_{\perp}(z, r=0) + i(\vec{v}_z \times \vec{B}_{\perp}) \right) e^{i\left(\frac{\omega_n z}{\beta c} + \varphi\right)} dz \right|^2}{\omega_n U} \Bigg|_{\max \varphi}$$

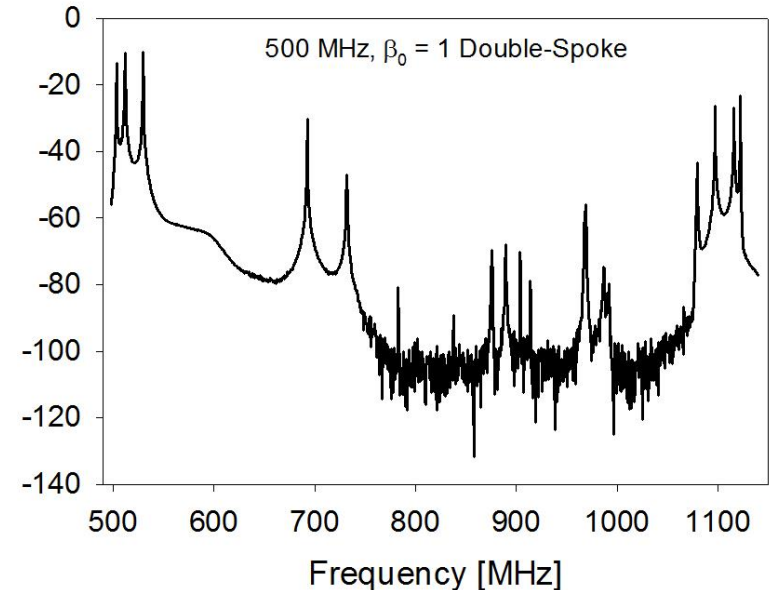
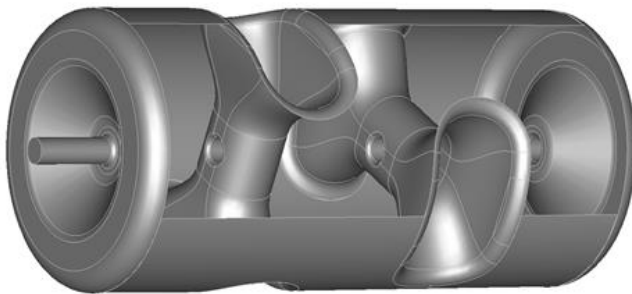
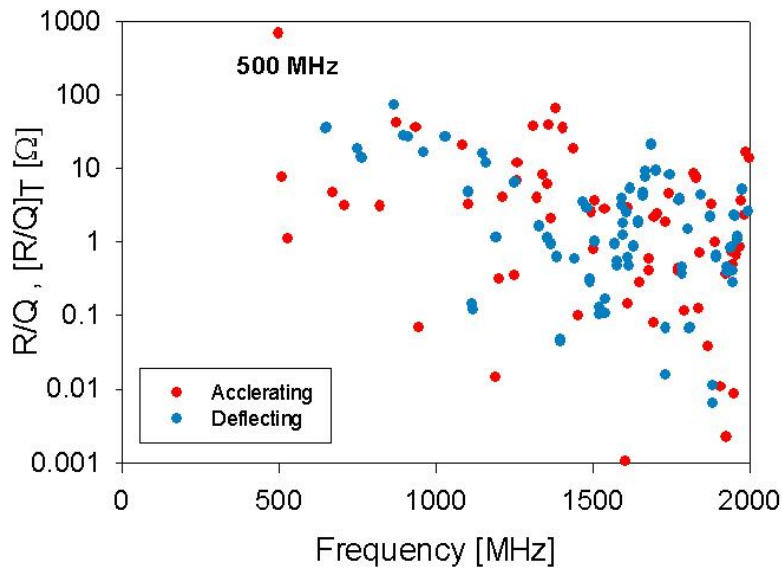
Verify with PWT

$$\Delta p_{\perp} = \left(\frac{e}{\omega_n}\right) \int_0^L (-i) \nabla_{\perp} E_z dz$$

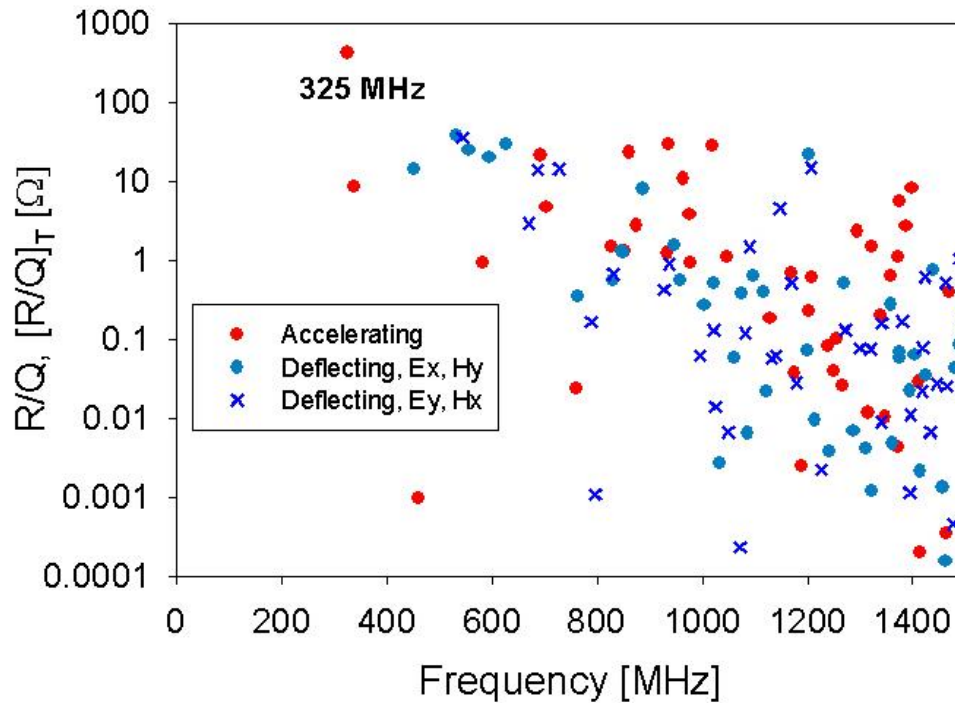
$$\left(\frac{R}{Q}\right)_{\perp} = \lim_{a \rightarrow 0} \frac{\left| \int_{-\infty}^{+\infty} \left( \vec{E}_{\perp}(z, r=0) + i(\vec{v}_z \times \vec{B}_{\perp}) \right) e^{i\left(\frac{\omega_n z}{\beta c} + \varphi\right)} dz \right|^2}{(k_n a)^2 \omega_n U} \Bigg|_{\max \varphi}$$

# [R/Q] VALUES OF HOMs

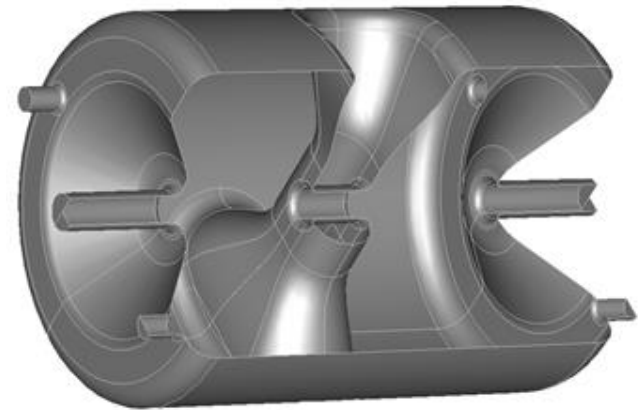
[R/Q] values for particles at design velocity  $\beta_0 = 1$  for the 500 MHz double-spoke cavity



# [R/Q] Values of HOMs



[R/Q] values for particles at design velocity  $\beta_0 = 0.82$  for the 325 MHz single-spoke cavity

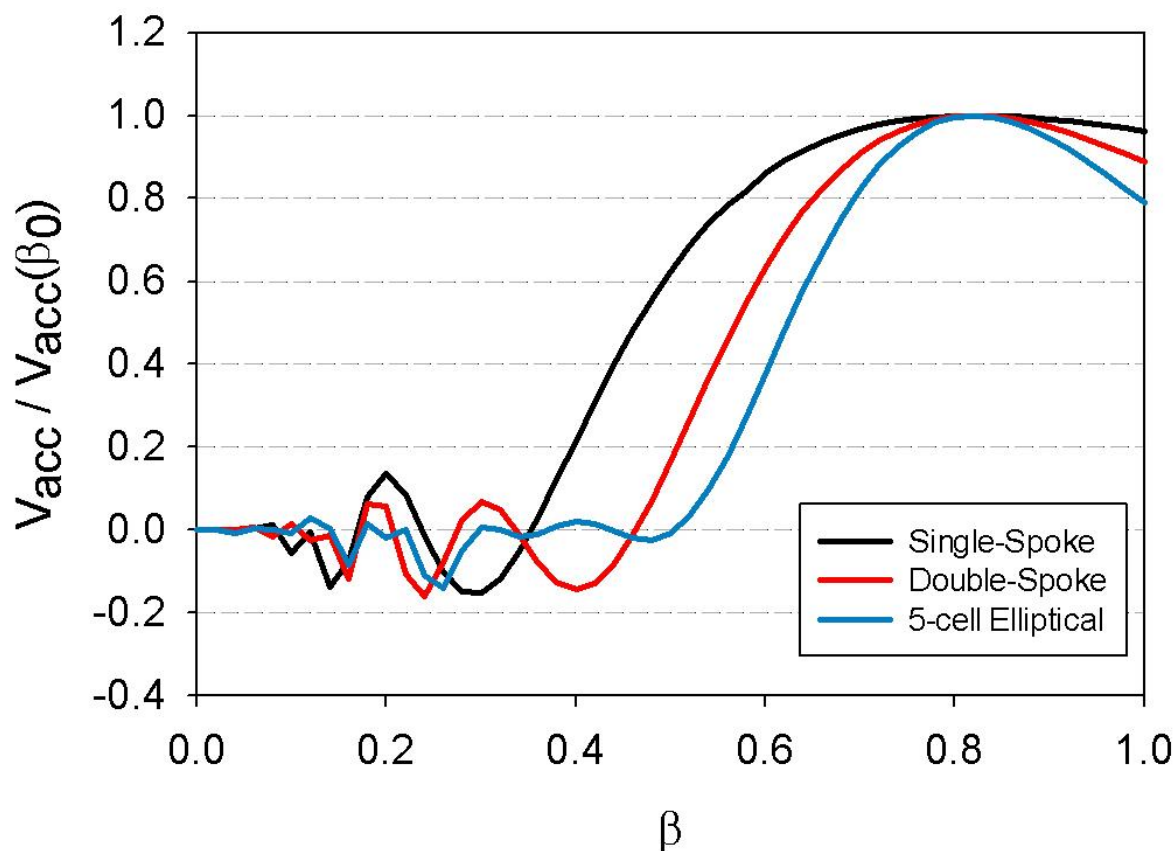


325 MHz,  $\beta_0 = 0.82$  single-spoke cavity

- Introduction
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- $[R/Q]$ ,  $[R/Q]_T$  Calculations
- **Velocity Dependence**
- HOM Damping

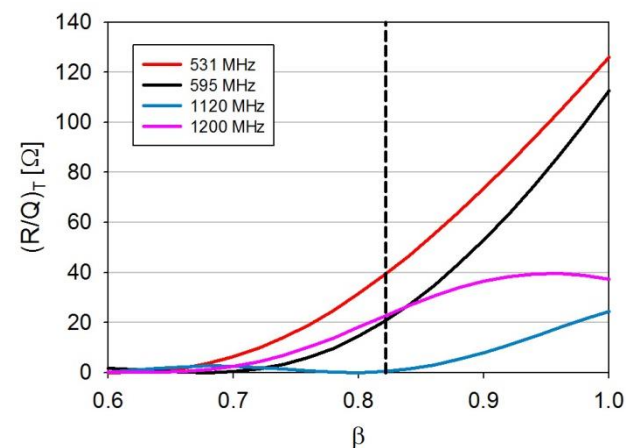
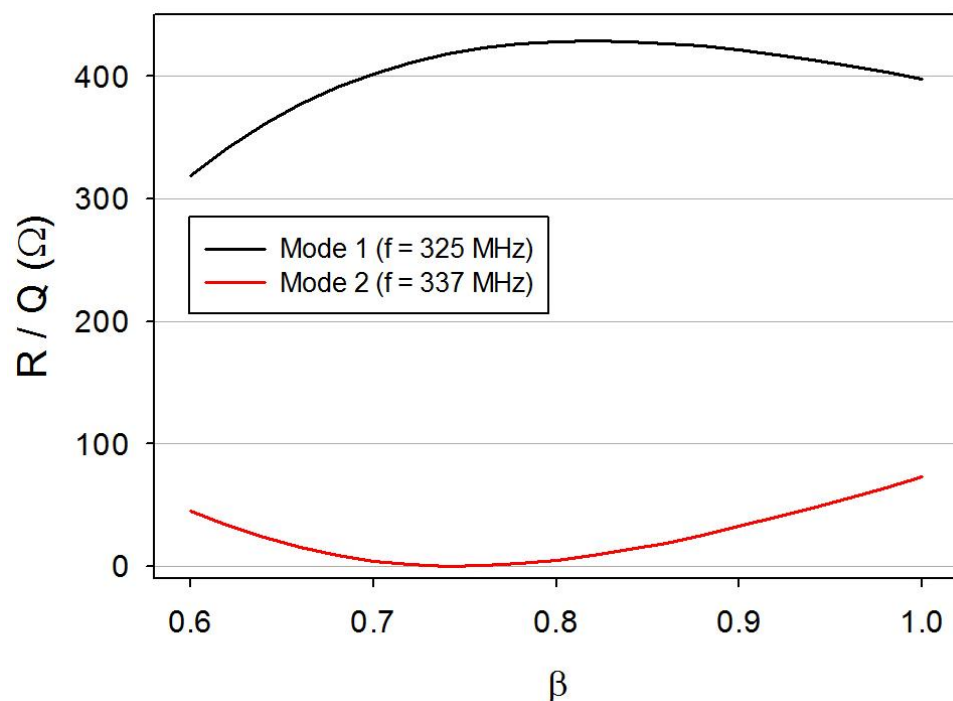
# VELOCITY ACCEPTANCE

- Single-spoke cavity: Greater than 96% efficiency between  $0.7 \leq \beta \leq 1$ .
- This corresponds to protons with energies between 380 MeV and  $> 1.5$  GeV
- Double-spoke cavity: Greater than 96% efficiency between  $0.74 \leq \beta \leq 0.92$ .
- This corresponds to protons with energies between 460 MeV and 1.5 GeV

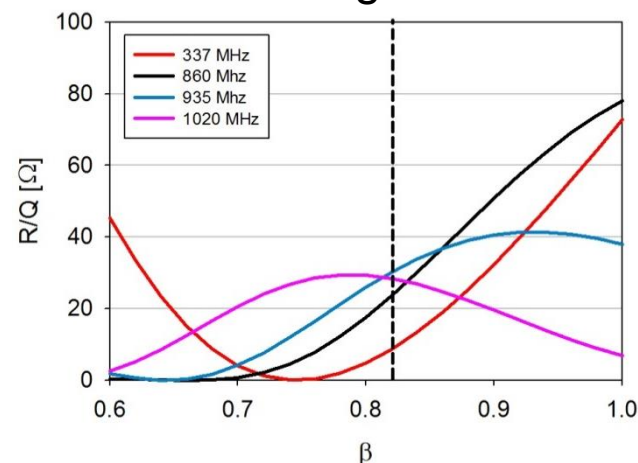


# VELOCITY DEPENDENCE (SINGLE-SPOKE)

325 MHz,  $\beta_0 = 0.82$  single-spoke  
cavity ( $R/Q = 450 \Omega$ )



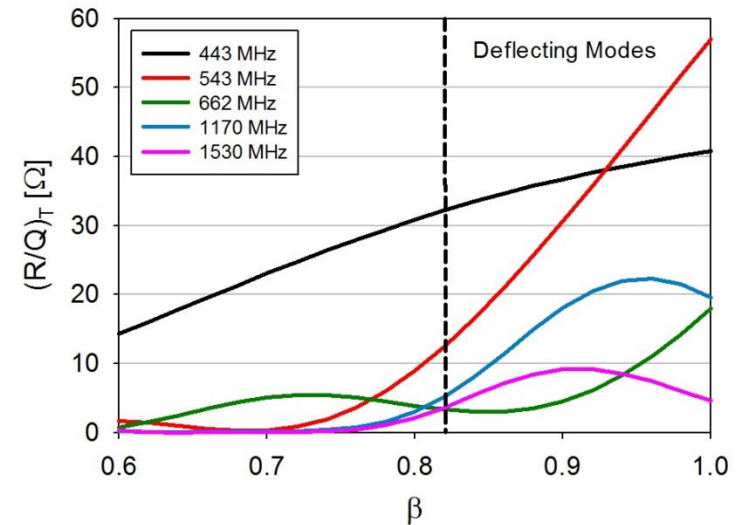
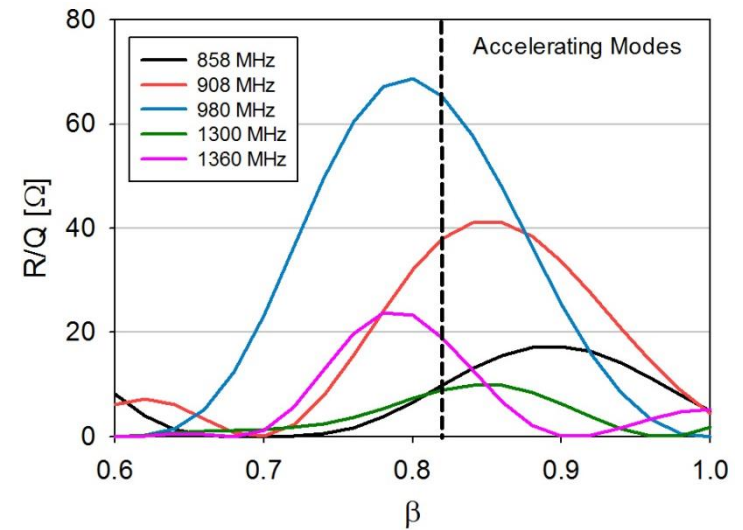
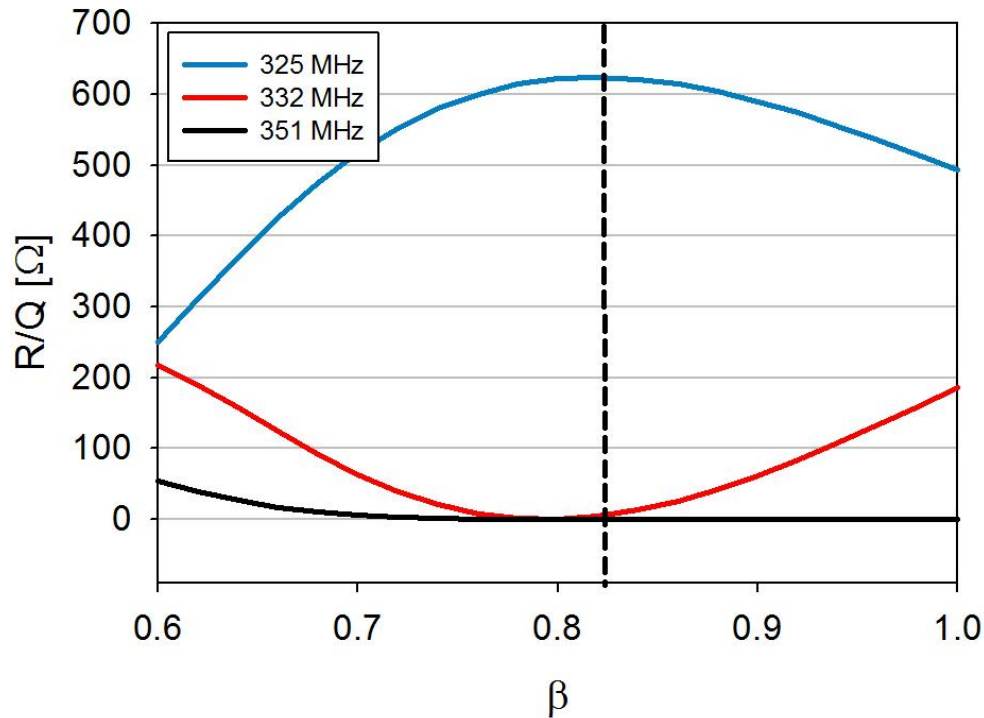
Deflecting Modes



Accelerating Modes

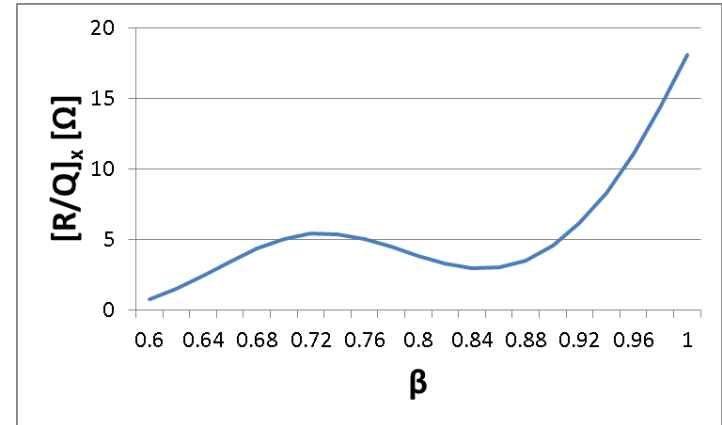
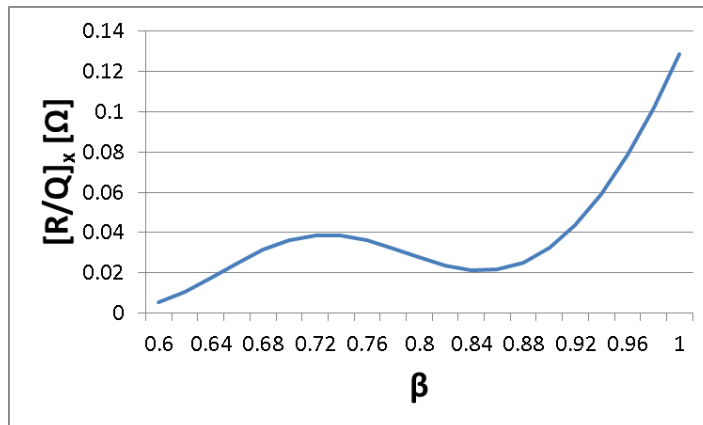
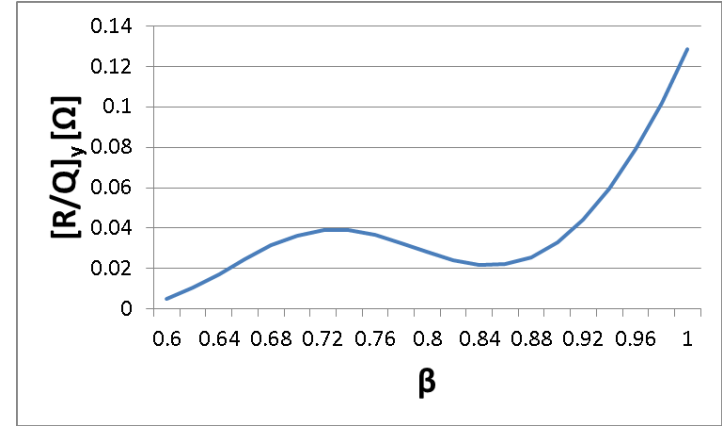
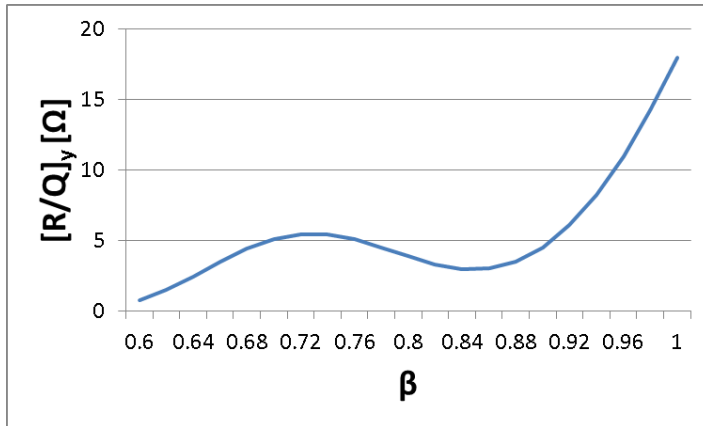
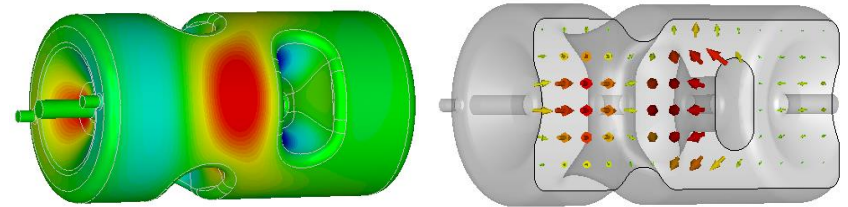
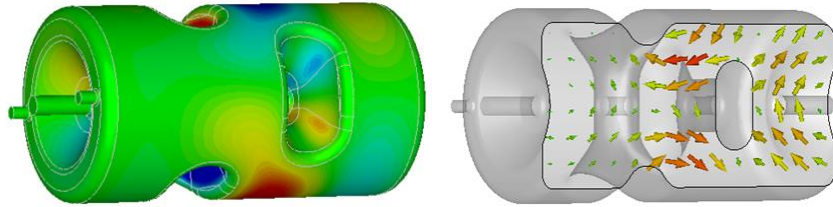
# VELOCITY DEPENDENCE (DOUBLE-SPOKE)

325 MHz,  $\beta_0 = 0.82$  double-spoke cavity  
( $R/Q = 625 \Omega$ )



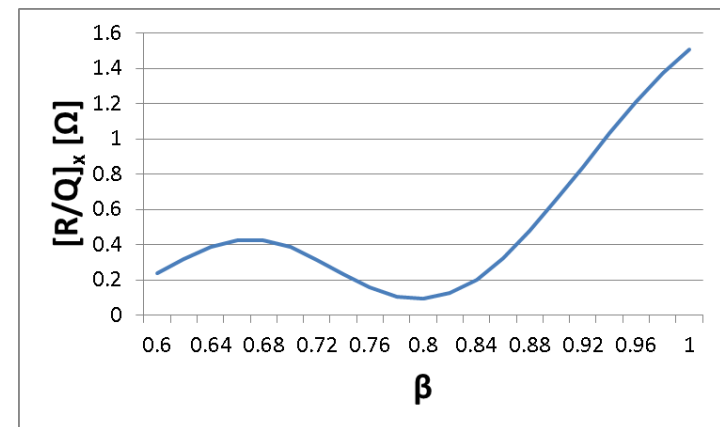
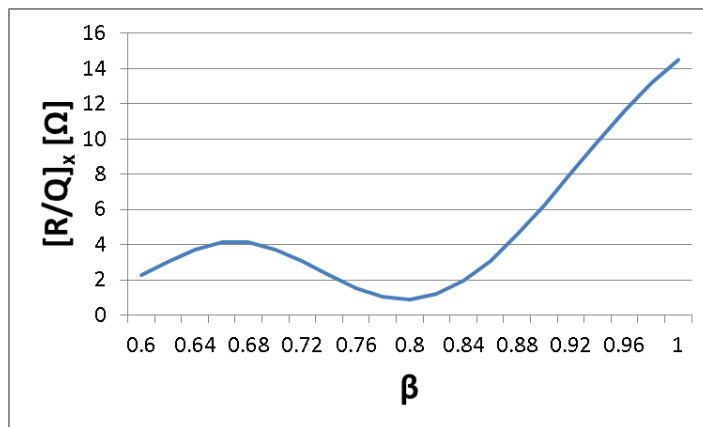
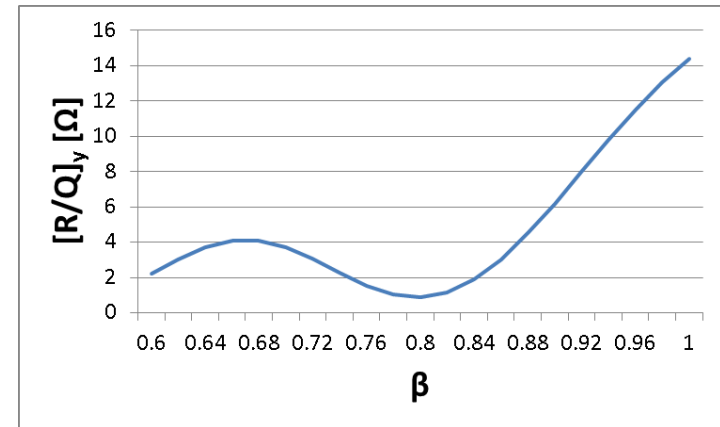
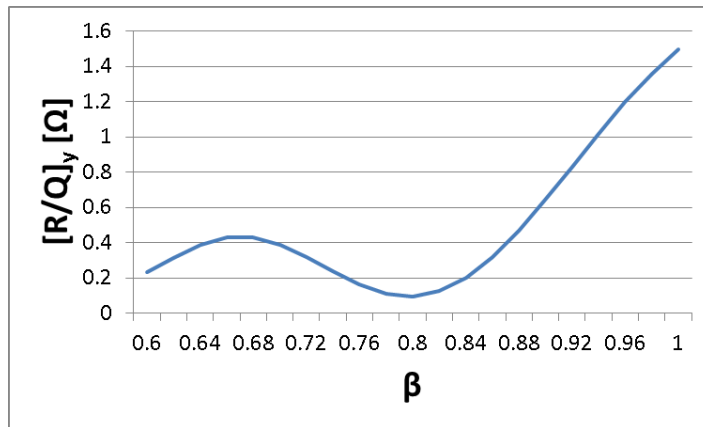
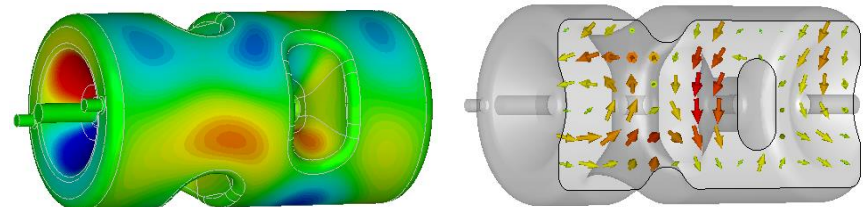
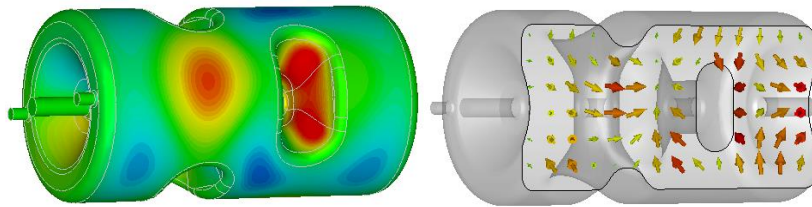


# $f = 662 \text{ MHz}$ DEGENERATE MODE

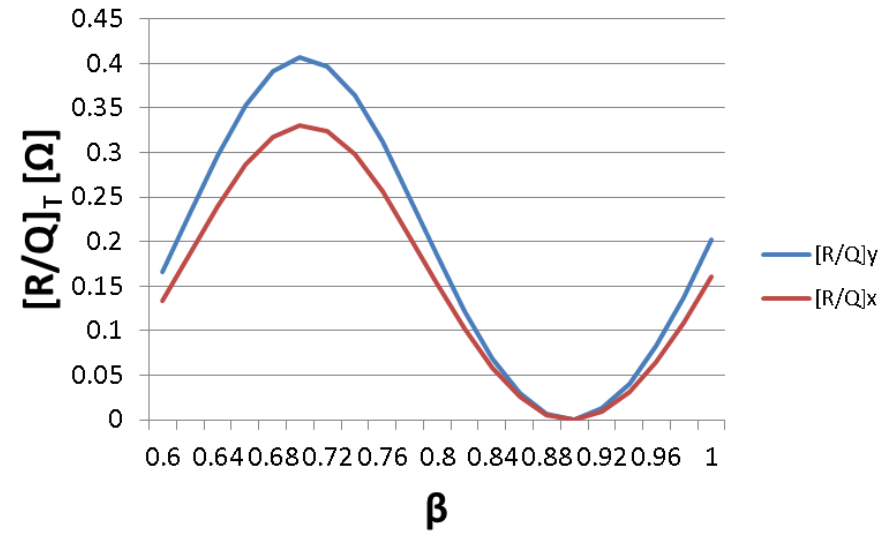
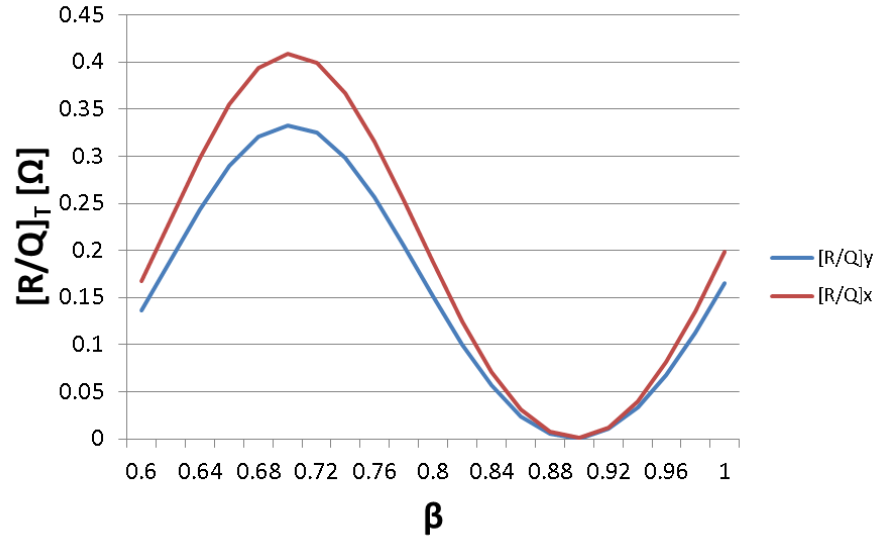
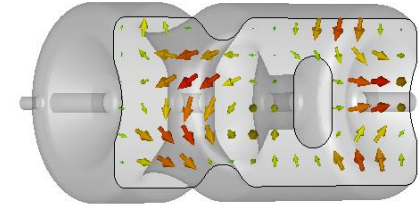
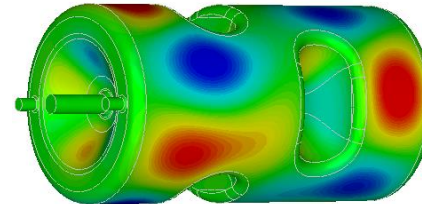
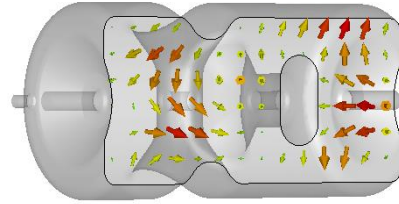
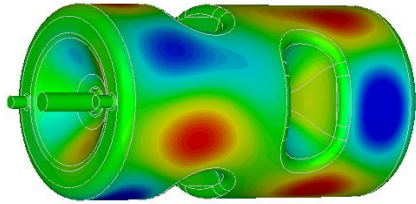




# $f = 727 \text{ MHz}$ DEGENERATE MODE



# $f = 770$ MHz DEGENERATE MODE



- Introduction
- Mode Types
- $[R/Q]$ ,  $[R/Q]_T$  Calculations
- Velocity Dependence
- **HOM Damping**

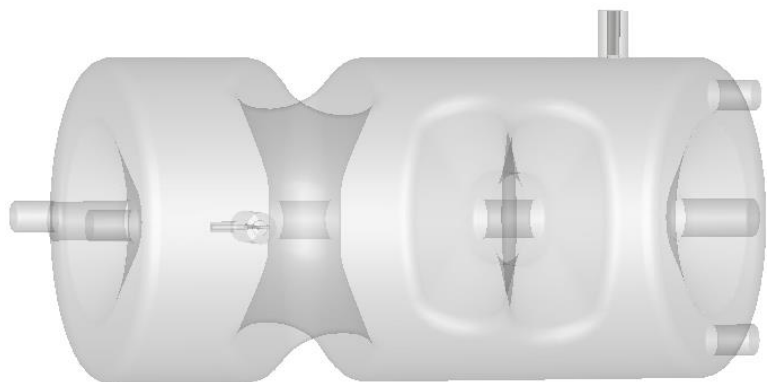
# 500 MHz $\beta_0 = 1$ DOUBLE-SPOKE

- Compact light source using 4 double-spoke cavities to accelerate electrons from 2 – 25 MeV
- Prototype currently being fabricated in an ODU/Jlab collaboration.

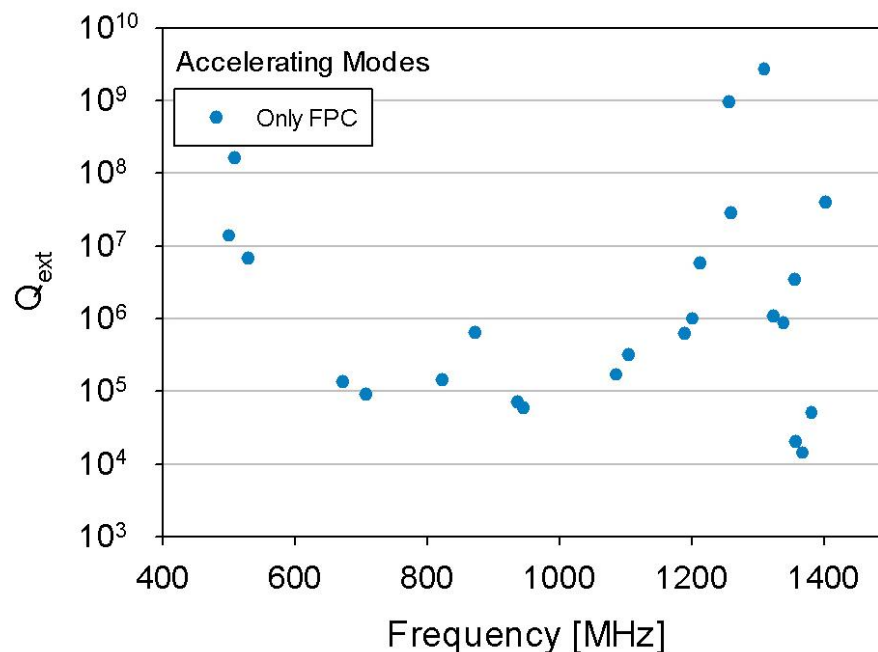
Parameter	Value	Units
Bunch Charge	10	pC
Rep. Rate	100	MHz
$f_{rf}$	500	MHz
Beam Current	1	mA
Bunch Length	0.9 (3)	mm (psec)
Cavity Voltage $V_{acc}$	6	MV
Quality Factor $Q_0$	$1.5 \times 10^9$	-



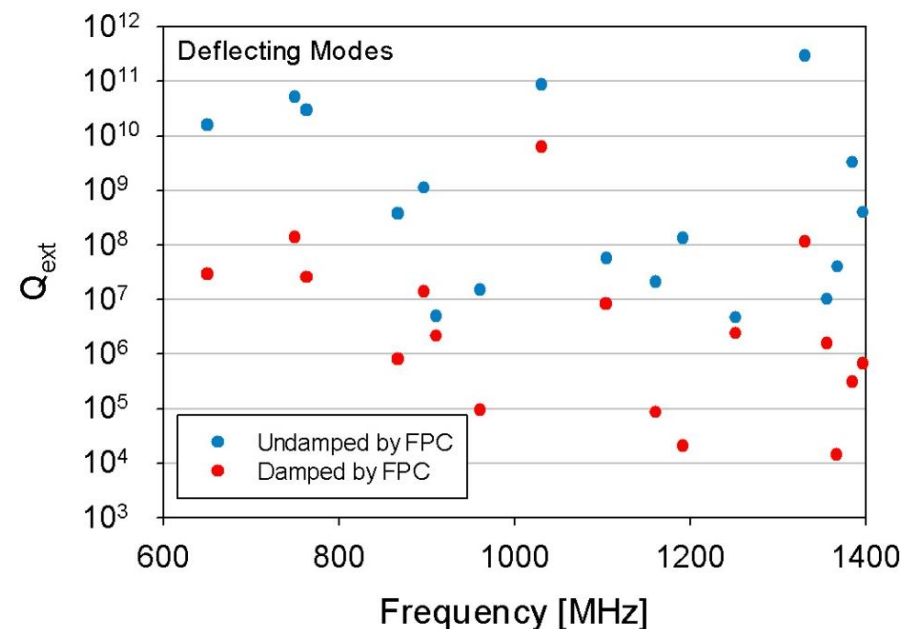
# FUNDAMENTAL POWER COUPLER



The optimal loaded quality factor is  $\sim 1 \times 10^7$ .

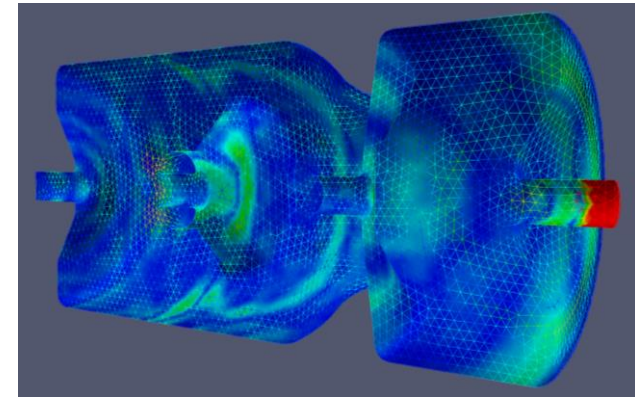


Some HOMs strongly couple to the FPC, however the load is only matched to the fundamental mode.

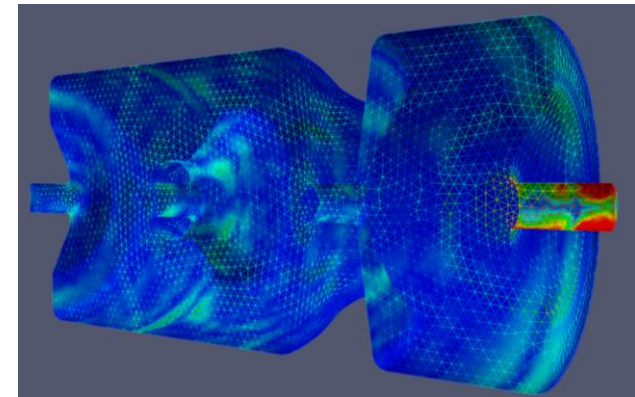


# UNDAMPED MODES

Frequency [MHz]	(R/Q) [ $\Omega$ ]	$Q_{\text{ext}}$
1256	7	$9 \times 10^8$
1260	12	$2.7 \times 10^9$
1310	38	$2.8 \times 10^7$
1403	36	$4 \times 10^7$



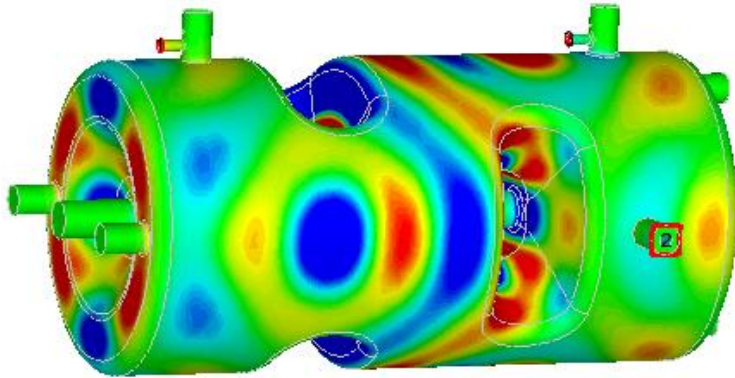
Frequency [MHz]	(R/Q) [ $\Omega$ ]	$Q_{\text{ext}}$
650	36	$1.6 \times 10^{10}$
749	19	$5.2 \times 10^{10}$
763	16	$3 \times 10^{10}$
897	28	$1.1 \times 10^9$
1030	27	$8.7 \times 10^{10}$





# SURFACE FIELDS

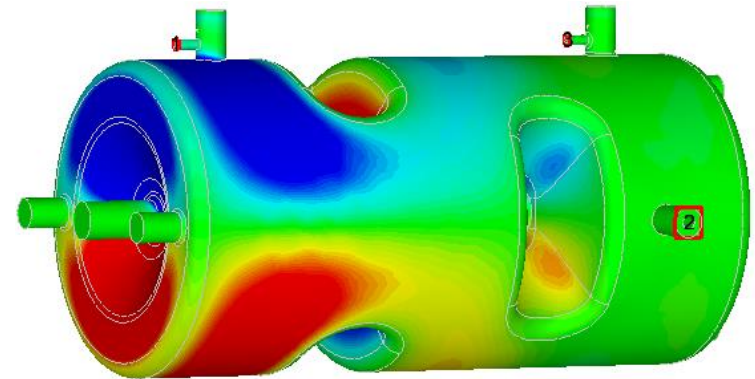
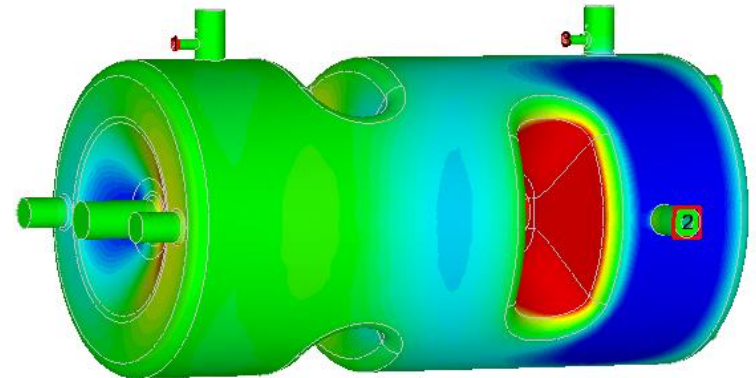
Surface electric field



**1999 MHz Accelerating Mode**

Various coupler placements need to be tried to effectively couple to the most dangerous modes

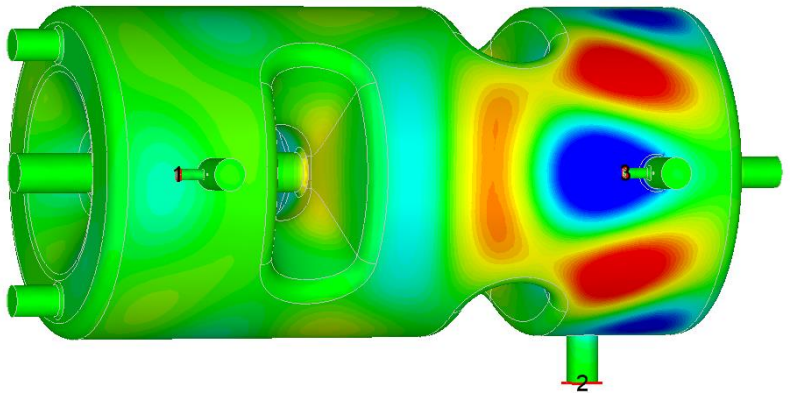
Surface electric field



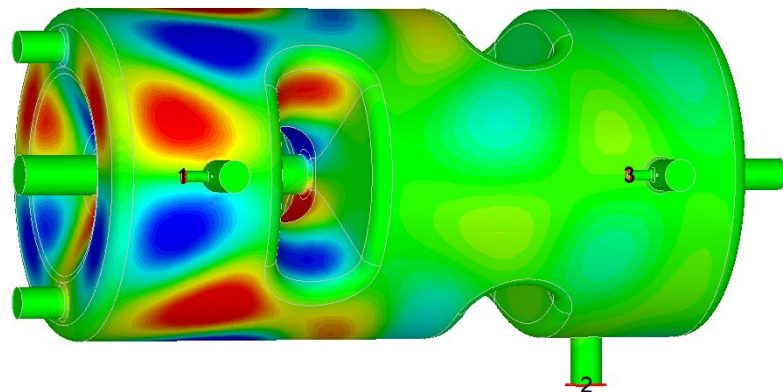
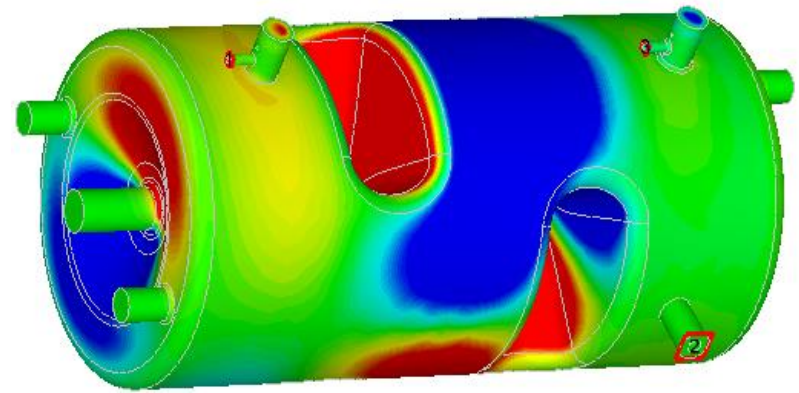
**897 MHz Deflecting Mode**

# SURFACE FIELDS

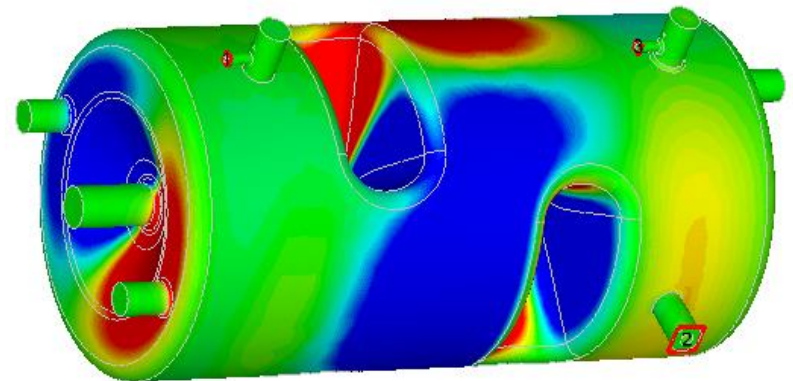
Surface electric field



Surface electric field



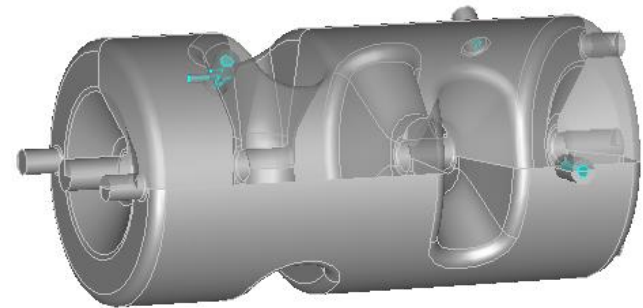
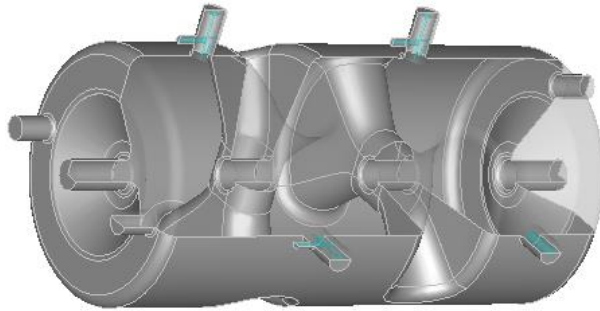
1569 MHz Deflecting Mode



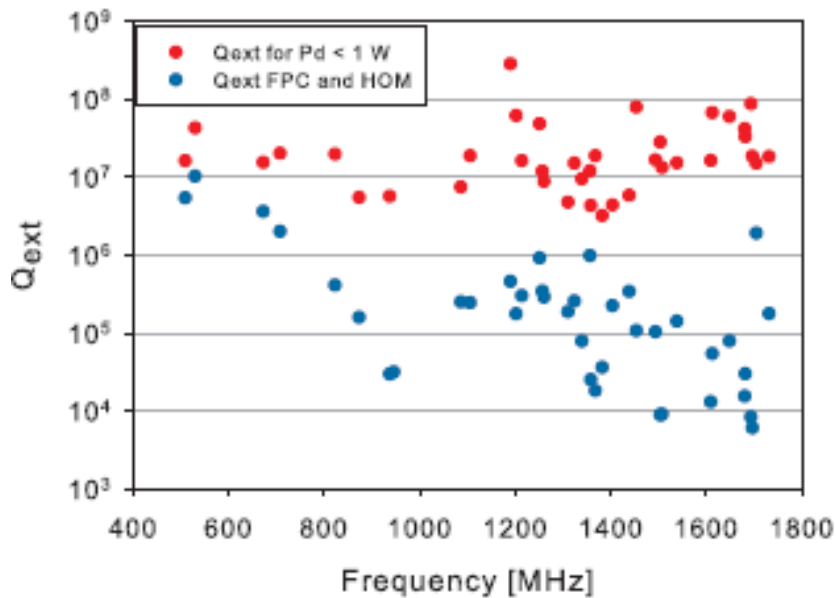
911 MHz Deflecting Mode



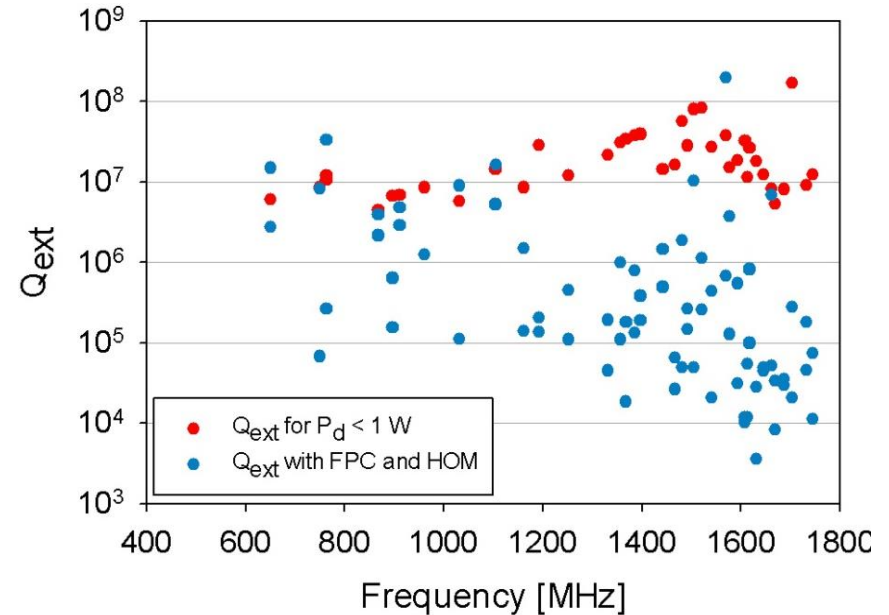
# HOM DAMPING



- Moderate damping to keep the cryogenic losses due to HOMs “tolerable.”



Accelerating modes



Deflecting modes

# CONCLUSIONS

- Multi-spoke cavities have a complex HOM spectrum
- Symmetry leads to deflection not along one axis
- Both single- and multi-spoke cavities offer a great deal of flexibility in terms of coupler placement (no need to introduce asymmetries to couple in certain areas)
- Many questions still to be explored:
  - What are the beam dynamics and how can the orientation of the spokes be used in our favor?
  - Coupler configurations for most effective damping
  - How will cavity tuning affect HOM spectrum

# ACKNOWLEDGEMENTS

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- ODU
  - Prof. Jean Delayen
  - Subashini De Silva
  - Alex Castilla
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- Muons, Inc.
  - Frank Marhauser
- SLAC
  - Zenghai Li
- LANL
  - Frank Krawczyk